

## 10. Phase Transformations

Homework Chapter 9, Prob. 2, 5  
Chapter 10, Prob. 1, 2, 3, 5

Phase transitions: Most active subset of research in modern statistical physics

Basic phenomenon — small change in a variable (e.g.  $T$ ) causes large qualitative change in equilibrium configuration

Examples:

- Water (at  $P = 1 \text{ atm}$ )
  - ice-liquid at  $0^\circ \text{C}$
  - liquid-steam at  $100^\circ \text{C}$
- Conductor-insulator transition
- onset of Ferromagnetism (iron won't magnetize above critical temp)
- Superfluidity ( $2.17^\circ \text{K}$  in  $^4\text{He}$ )
- Superconductivity ("High- $T_C$ ")

Mathematics:

Hallmark of phase transition is discontinuous behavior (of e.g. density as a function of  $T$ )

$$Z = \sum_{\text{states}} e^{-E_{\text{state}}/T}$$

must have discontinuous derivatives

this means that sum must be infinite  
 strictly speaking, phase transitions can occur only  
 for volume  $V \rightarrow \infty$ .  
 in practice - rounding of discontinuity due to  
 finite volume may be unobservable.

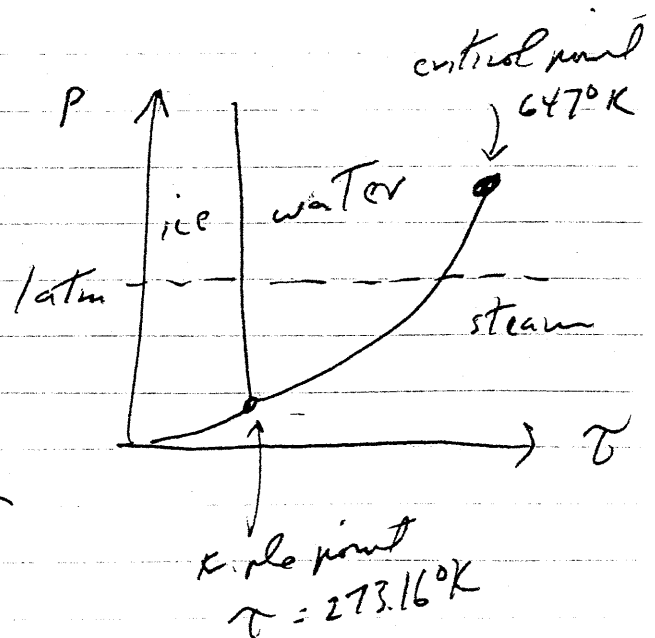
Two things to investigate:

- 1) How much can we understand about phase transitions using thermodynamics, without worrying about details of a microscopic picture
- 2) How do we understand phase transitions from a fundamental, microscopic point of view. E.g. cobalt  $T_{crit}$ , etc. from first principles

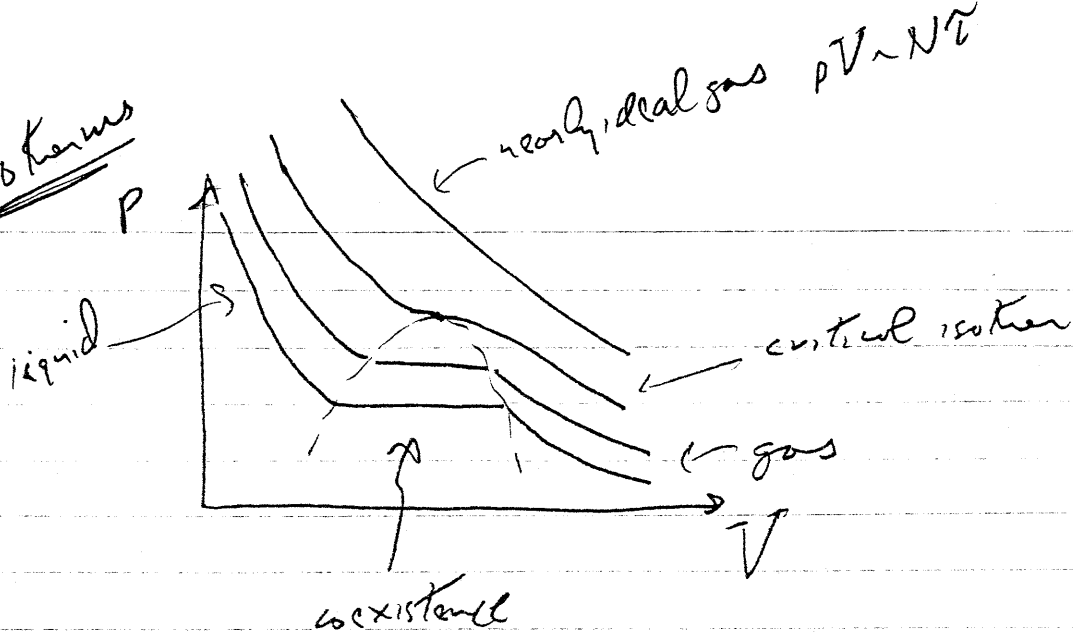
### Coexistence of Phases

Example: 3 phases of water  
 At given pressure, 2 phases can be in stable contact (in equilibrium) only at particular transition temperatures.

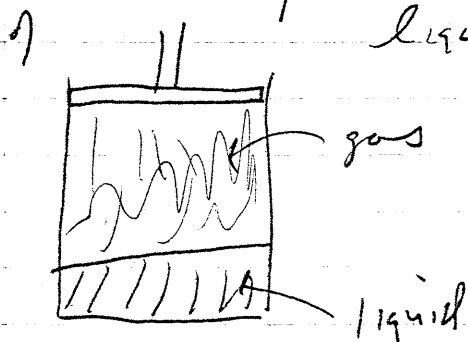
Or - fix  $T$  and vary available volume -



156 terms



(At sufficiently high  $T$  (or  $p$ ) there is no coexistence liquid and gas)



At given  $T$ , liquid coexists with vapor at a particular pressure

Gas and liquid are in --

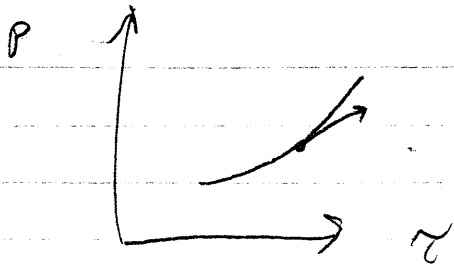
- thermal equilibrium (same  $T$ ) - or heat would flow
- mechanical equilibrium (same  $p$ ) - or boundary would move  $\Delta V$
- diffusive equilibrium (same  $\mu$ ) - or else  $N$  flows

### Coexistence Curve

How does  $p$  at coexistence vary with  $T$ ?

$$\mu_L(p, T) = \mu_g(p, T)$$

— one condition determines a curve in  $p-T$  plane. Find slope of the curve.



$$\mu_g(p+dp, \tau+d\tau) = \mu_l(p+dp, \tau+d\tau)$$

$$\approx \left(\frac{\partial \mu_g}{\partial p}\right)_\tau dp + \left(\frac{\partial \mu_g}{\partial \tau}\right)_p d\tau$$

$$= \left(\frac{\partial \mu_l}{\partial p}\right)_\tau dp + \left(\frac{\partial \mu_l}{\partial \tau}\right)_p d\tau$$

$$\Rightarrow \left[ \left(\frac{\partial \mu_l}{\partial \tau}\right)_p - \left(\frac{\partial \mu_g}{\partial \tau}\right)_p \right] d\tau = \left[ \left(\frac{\partial \mu_g}{\partial p}\right)_\tau - \left(\frac{\partial \mu_l}{\partial p}\right)_\tau \right] dp$$

$$\Rightarrow \left(\frac{dp}{d\tau}\right)_{\text{coex}} = \frac{\left(\frac{\partial \mu_l}{\partial \tau}\right)_p - \left(\frac{\partial \mu_g}{\partial \tau}\right)_p}{\left(\frac{\partial \mu_g}{\partial p}\right)_\tau - \left(\frac{\partial \mu_l}{\partial p}\right)_\tau}$$

Recall Gibbs free energy (Chapter 9)

$$G(\tau, p, N) = N \mu(\tau, p)$$

and  $\left(\frac{\partial G}{\partial p}\right)_{\tau, N} = V$ ,  $\left(\frac{\partial G}{\partial \tau}\right)_{p, N} = -S$

If we denote  $v = V/N$   $s = S/N$

volume  
and entropy  
per particle

then  $\left(\frac{dp}{d\tau}\right)_{\text{coex}} = \frac{s_g - s_l}{v_g - v_l}$

Can relate  $\Delta S$  to Latent Heat

$Q = \tau \Delta S$  or  $L = \tau \Delta S$  is amount of heat (per particle) required to boil the liquid

So  $\left(\frac{dp}{dT}\right)_{\text{coex}} = \frac{L}{T\Delta V}$  the Clausius-Clapeyron eqn (which is well verified)

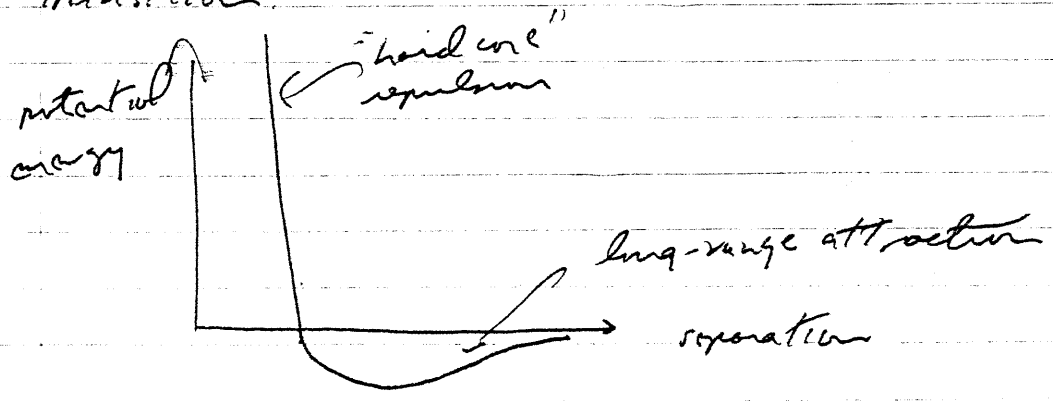
this applies to water-ice transition as well. Note:  $\Delta V < 0$  (ice floats)  $\Delta S > 0$  (need heat to melt ice)

Hence  $(dp/dT)_{\text{coex}} < 0$ .

pressure lowers the coexistence temperature (unusual) which is why we can skate on ice.

Vander Waal's Equation of State (1873)

We'll consider how interactions among gas molecules modify the ideal gas relation  $pV = NkT$ . This will lead us to a crude model of the gas-liquid phase transition.



Effect of the hard core:  $V \rightarrow V - Nb$   
 exclude some volume ( $b = \text{vol. per particle}$ )

Effect of the attraction:

$$U = \sum_{\text{pairs}} V_{\text{pair}} = \frac{1}{2} \int d^3x d^3y n(\vec{x}) n(\vec{y}) V(\vec{x}-\vec{y})$$

Assume density is uniform,  $n = \text{constant}$   
 ("Mean field theory" - ignores density fluctuations)

$$= n^2 V \int \frac{1}{2} d^3x V(\vec{x}) = -a N^2 / V$$

Contribution to the pressure  $p \approx -\frac{\partial U}{\partial V} = -a N^2 / V^2$

(attractive)  
 $\Rightarrow a > 0$

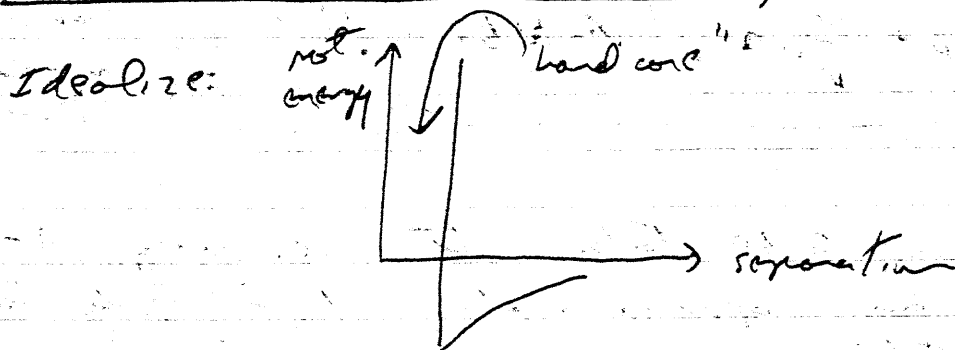
So —  $pV = N\tau$

$$\Rightarrow \left( p = \frac{N\tau}{V-Nb} - a \frac{N^2}{V^2} \right)$$

Vander Waals  
 equation

- This is reasonable approximation when gas is close to ideal ( $n = N/V$  sufficiently small)
- But we will use it (without justification) even when corrections to ideal behavior are big (e.g., when gas liquefies)

# Van der Waals Equation of State



Effect of hard core: excluded volume  
 $V \rightarrow V - Nb$      $b = \text{vol per particle}$

Effect of attraction

$$\Delta U = \sum_{\text{pairs } \langle ij \rangle} V_{ij}$$

$$= \frac{1}{2} \int d^3x d^3y n(\vec{x}) n(\vec{y}) V(\vec{x}-\vec{y})$$

"Mean field theory" - treat density  $n$  as uniform, ignoring fluctuations

$$= \frac{1}{2} n^2 V \int d^3x V(\vec{x}) = -a \frac{N^2}{V}$$

( $a > 0$ , because pot. energy is negative)

Some write

$$F_{vdw} = F_{ideal}(V - Nb) - a \frac{N^2}{V}$$

$$= -N\tau \log \left[ n_Q \left( \frac{V - Nb}{N} \right) \right] - a \frac{N^2}{V}$$

pressure

$$P = - \left( \frac{\partial F}{\partial V} \right)_{T, N} = \frac{N\tau}{V - Nb} - \frac{N^2}{V^2} a$$

(over)

We have

$$\left( p + \frac{N^2}{V^2} a \right) (V - Nb) = N \tau$$

van der  
Waals eqn of  
state

It is not to be taken too seriously. At best an approximation that applies to sufficiently dilute gas. Without justification, we will apply it to dense gas



For given  $\tau$  and  $p$ , what is  $V$ ?  
 solve a cubic equation

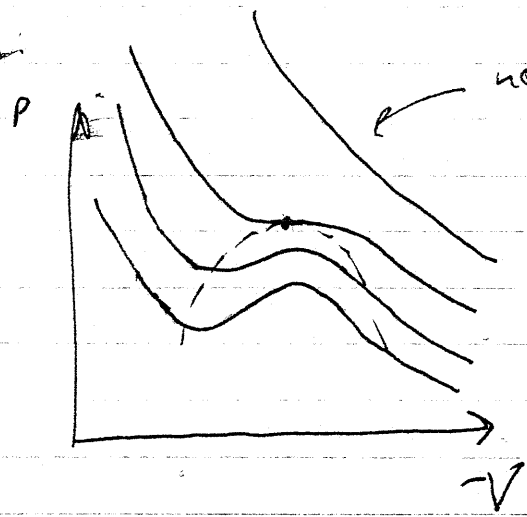
$$\left(V^2 + \frac{N^2 a}{P}\right)(V - Nb) = \frac{N \tau V^2}{P}$$

(we multiply vdW eqn by  $V^2/P$ )

$$a V^3 - \left(Nb + \frac{N \tau}{P}\right) V^2 + \frac{N^2 a}{P} V - \frac{N^3 ab}{P} = 0$$

Has either one or 3 real solutions

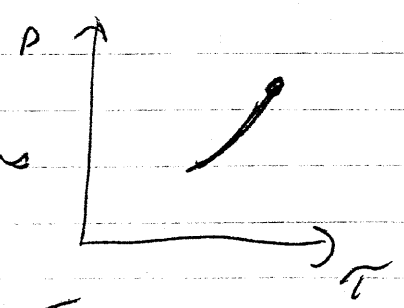
Isotherms



NOTE:  $\tau$   
 $\rightarrow \tau_c \Rightarrow$   
 $V_c = N \tau_c / P$  is  
 approx. soln.

This is critical point where the  
 multivaluedness  
 of  $V$  turns on

As we'll soon see, can  
 regard  $p_c, \tau_c$  as end of line  
 of first-order phase transitions  
 in  $p-\tau$  plane



Let's solve for  $p_c, \tau_c, V_c$  in terms  
 of  $N, a, b$

At critical point:  $(V - V_c)^{3/2} = 0$   
 eqn of state has 3 degenerate solutions

expand:  $V^3 - 3V_c V^2 + 3V_c^2 V - V_c^3 = 0$

Equate:

①  $3V_c = Nb + N\tau_c / p_c$

②  $3V_c^2 = \frac{N^2 a}{p_c}$

③  $V_c^3 = \frac{N^3 ab}{p_c}$

Divide ③ by ②:  $V_c / 3 = Nb$  or  $V_c = 3Nb$   
 (three times excluded volume)

②  $\Rightarrow 27N^2 b^2 = N^2 a / p_c$   
 $\Rightarrow p_c = \frac{a}{27b^2}$

①  $\Rightarrow \tau_c = p_c / N (3V_c - Nb) = \frac{a}{27b^2} 8b = \frac{8a}{27b} = \tau_c$

Now we can eliminate a, b, N and express vdW eqn in terms of  $V_c, p_c, \tau_c$

$\left(\frac{V}{V_c} - \frac{Nb}{V_c}\right) \left(\frac{p}{p_c} + \frac{V_c^2 N^2 a}{V^2 V_c^2 p_c}\right) = \frac{\tau}{\tau_c} \frac{N\tau_c}{V_c p_c}$

$Nb/V_c = 1/3; \quad \frac{N^2 a}{V_c^2 p_c} = \frac{a}{9b^2} \frac{27b^2}{a} = 3$

$\frac{N\tau_c}{V_c p_c} = \frac{8a}{27b} \frac{1}{36} \frac{27b^2}{a} = 8/3$

We have

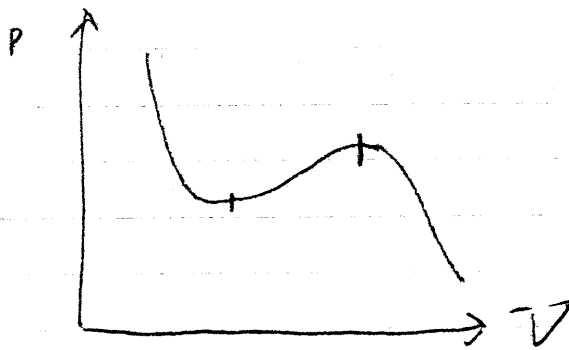
$$\left( \frac{V}{V_c} - \frac{1}{3} \right) \left( \frac{p}{p_c} + 3 \left( \frac{V}{V_c} \right)^2 \right) = \frac{8}{3} \frac{\tau}{\tau_c}$$

- "The Law of Corresponding States"

Correction to ideal gas law takes "universal" form (same for all gases) when expressed in terms of critical values.

Doesn't work all that well, nor should it

### The Maxwell Construction



Consider system for  $\tau < \tau_c$

Here is a region with

$$dp/dV > 0$$

what is significance of this?

(Note  $\kappa_T \equiv -\frac{1}{V} \left( \frac{dV}{dP} \right)_T$  = "compressibility")

### Instability

Mathematically: system + reservoir choose volume  $V$  to minimize Helmholtz free energy  $F$

$$\text{so } dF = \left[ \left( \frac{\partial F_{\text{sys}}}{\partial V} \right)_T - \left( \frac{\partial F_{\text{res}}}{\partial V} \right)_T \right] dV_{\text{sys}} = 0$$

$$\text{so } p_{\text{sys}} = p_{\text{res}} \quad \left( p = - \left( \frac{\partial F}{\partial V} \right)_T \right)$$

But for this to be minimum, need  $d^2F \geq 0$

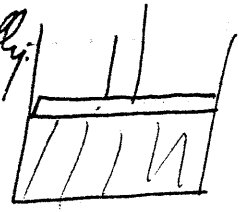
(over)

$$-\frac{\partial}{\partial V_{sys}} (P_{sys} - P_{res}) > 0$$

and  $\frac{\partial P_{res}}{\partial V} \approx 0$

so  $-\frac{\partial P}{\partial V} > 0$

physically:



If we push a little harder, system pushes back less hard  $\Rightarrow$  it will collapse

Incidentally, a similar stability criterion applies to heat transfer

$$dS = \left[ \left( \frac{\partial S_{sys}}{\partial U} \right)_V - \left( \frac{\partial S_{res}}{\partial U} \right)_V \right] dU_{sys}$$

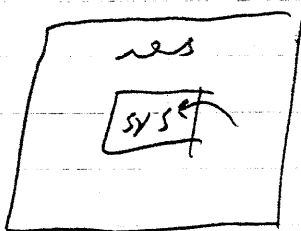
$$= \left( \frac{1}{T_{sys}} - \frac{1}{T_{res}} \right) dU_{sys} \Rightarrow T_{sys} = T_{res}$$

But  $d^2S \leq 0$  needed, if entropy is maximized

$$\frac{\partial T_{res}}{\partial U} = 0$$

$$\text{so } \frac{\partial}{\partial U} \frac{1}{T} = -\frac{1}{T^2} \frac{\partial T}{\partial U} = -\frac{1}{T^2} C_V \leq 0$$

This requires  $C_V \geq 0$ ; heat capacity is positive

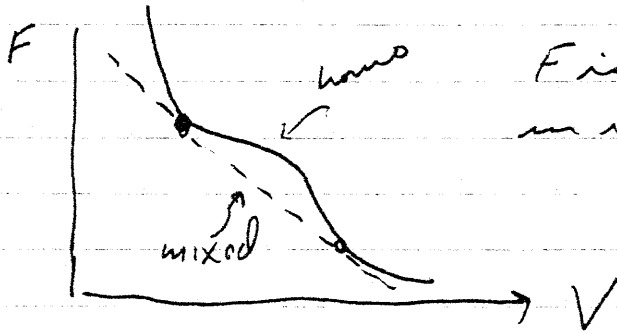
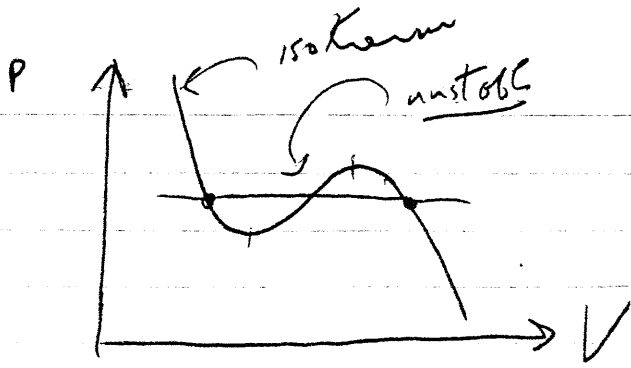


Physically -- if system has negative heat capacity, heat flow into the system cools it down, so more heat flows in.

unstable with respect to what? what state does the system prefer to be in?

To see this, consider  $F$  as a function of  $V$ , with  $T$  fixed.

$$F = - \int_{\text{isotherm}} p dV \quad (+ \text{ constant})$$



F is concave downward  
in region where  $dp/dV > 0$

Here  $F$  is the free energy of homogeneous phase, but we should consider alternative of inhomogeneous phase — i.e. divide available volume into two different phases (at same  $p$  and  $T$ )

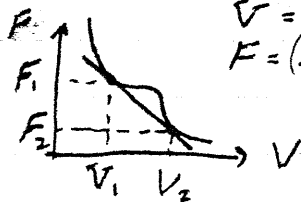
- Equating pressure means same slope for  $F$  vs  $V$  at both points

- Further  $F$  vs  $V$  in the mixed phase is

a straight line  $F = f_1 V_1 + f_2 V_2 = (f_1 - f_2) \Delta V + \text{const}$

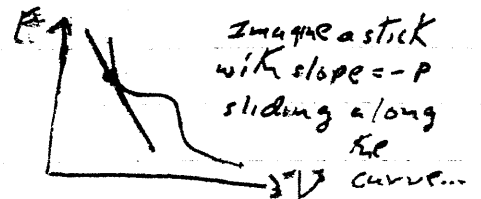
↑  
free energy per volume

When  $F$  is concave down, we can get lower  $F$  with a mixed phase — and lowest possible  $F$  along a line that is tangent to  $F(V)$  at two points as shown.

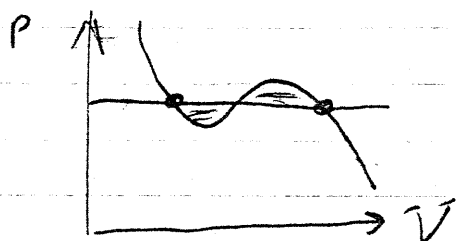


$$V = (1-\alpha)V_1 + \alpha V_2$$

$$F = (1-\alpha)F_1 + \alpha F_2$$



So... to find value of  $p(T)$  at



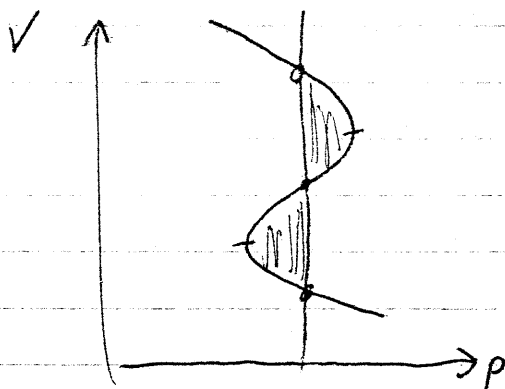
which coexistence occurs, we find slope of this common tangent

Since  $(\Delta F)_{\text{gas}} = (\Delta F)_{\text{liquid}}$ ,

we have 
$$\int (P)_{\text{gas}} dV = p \int dV$$

This means that regions above and below the horizontal line have equal areas.  
(Maxwell construction)

Another way to think about this:



Since the two phases are in diffusive equilibrium, they must have same chemical potential

So all gas and all liquid phases have same  $G = N\mu$

$$dG = V dp \Rightarrow \int V dp = 0$$

-again, equal areas

So... the gas and liquid phases have same  $G$  - but derivatives of  $G$  are not the same  $\rightarrow$  Defining property of "First-Order phase transition"